

## Review Article

### Wurster technology: Process variables involved and Scale up science

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## Abstract

Among the pelletization techniques available at present, wurster process is a production method of a great interest as it offers the various advantages in single equipment. Continuous process, less manual interruption and batch to batch reproducible assurance are some advantages of Wurster based pellets coating. The many scientist have no clarity that “is the process scalable?” due to ‘n’ number of process variables involves. There are five sets of process variables affecting the quality of pellets - Equipment variables, Coating liquid preparation variables, preheating variables, spraying variables and drying variable involved in Wurster based coating process. Many of them has medium and high risk. The risk need to reduced by studying the variables at lab level during development using quality by design (QbD) approach and experimental design software. Wurster basted coating process scale up possible based on complete optimization of process variables, understanding of risk associated with variables and implementation of scale up factor calculation provided by vendor. Lab scale and commercial scale Wurster should be linear and preferably of same manufacturer is the key of successfully implementation of scale up factor.

**Keywords:** pelletization techniques, wurster process, quality by design.

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## 1. Introduction

In recent years, a continuous interest has been focused on the development of formulations using multiparticulate systems, offering various advantages over single dosage forms, namely, an improved bioavailability (Abdul S et al., 2010, Mohamad A et al., 2006) easy administration for elderly people and for children (Varum FJ et al., 2011). These include a flexibility of blending of different release profile, reproducible gastric residence time, low risk of dose dumping, and low risk of high local drug concentration in the gastrointestinal tract ( Pan X et al., 2010, Tuleu C et al., 1999), low intra- and inter-subject variability in plasma levels and bioavailability (Dey NS et al., 2008), reduction of irritation of the gastric mucosa due to drug degradation of simple units (Abdul S et al., 2010, Bhad ME et al., 2010) and divided in to desired dose strengths without formulation

changes (Deb R et al., 2013). Pellets are so flexible intermediate that can fill in capsule, compressed to tablets, add in suspension or make lyophilized tablets. Commercially, there are three most accepted pelletization technologies i.e. Suspension/solution loading, powder loading and extrusion- spheronization. However suspension/solution loading is most accepted technology at industry level due continuous process, less manual interruption and batch to batch reproducible assurance.

Successful pellet coating process optimization at lab level using small capacity Wurster is half work done. Successful scale up of Wurster based coating process at commercial scale is a challenging task. The present review focuses on process variables involved in coating process and challenges in scale up of pellets from lab scale to industrial scale batch to get consistent results.

### Mechanism of Wurster coating process

The Wurster process widely use in the pharmaceutical industry powder coating and pellets coating. The Wurster containers available in the size that 100-500g to 800 Kg batch size can run. The Wurster process is used commercially for particles coating from less than 100 µm to tablets. The coating chamber of Wurster is typically slightly

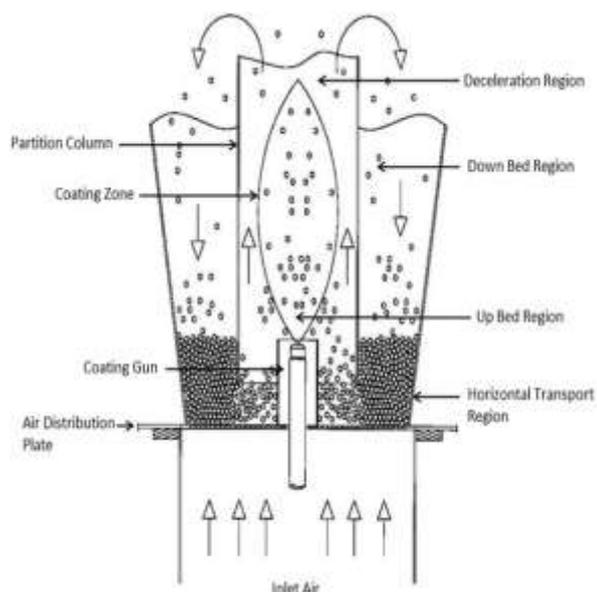


Figure 1: Schematic presentation of Wurster process

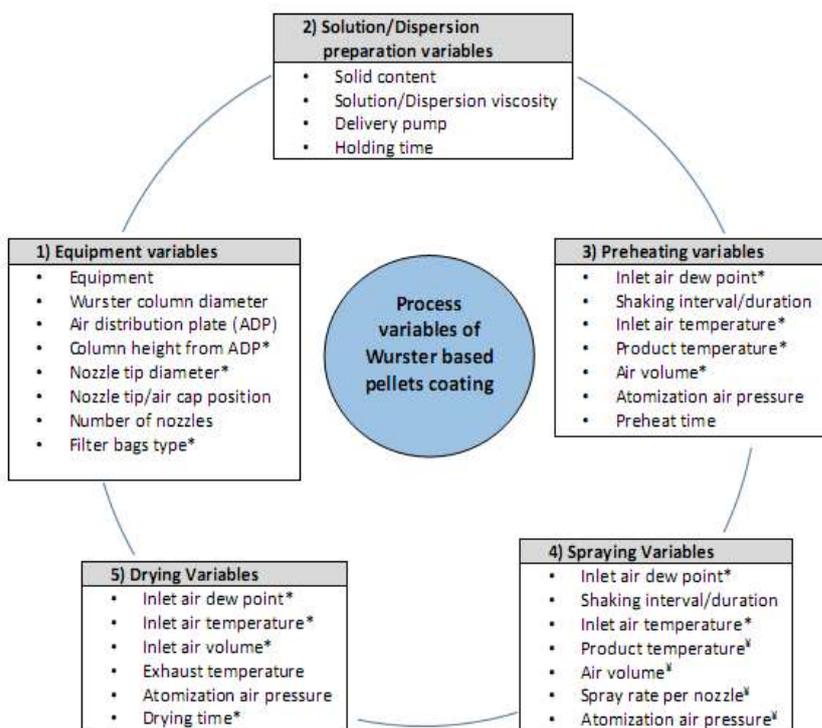
conical, and houses a cylindrical partition that is about half the diameter of the bottom of the coating region. At the bottom region, air distribution plates (ADP) also know as orifice plate accommodated. ADP divided in to two regions. The open area of the plate that is under the Wurster column is more permeable to allow more air volume and air velocity transport parallel to air flow. As inlet air accelerate upward, particles pass a spray nozzle that is mounted in the center of this up bed ADP. The nozzle is a binary type - one port of nozzle for liquid while other for atomized air at predecided volume and pressure. The spray pattern is in a solid cone of droplets, with a spray angle approximately 30–50° called as coating zone. Down bed is the

region outside the partition. The ADP selected based on size and density of material used.

The air flow in the down bed region keep material in suspended form and drawn horizontally into the gap at the base of the partition. The height of column controls the rate of substrate flow horizontally into the coating zone. During coating in progress, mass increased gradually so height of column increased to achieve desire pellets flow. Above the product container is the expansion area, which is typically conical to allow for decreasing air and particle velocity.

All fluidized-bed techniques are known for high rates of heat and mass transfer, and the Wurster process is very effective in this regard. Highly water-soluble materials can be coated using water-based applications without concern for core penetration. Droplets applied to the surface spread, and form a continuous film and rapidly dry. After a initial coat has been applied, increased the spray rates. Films formed from organic solvents base coating has high in quality, because the formed droplets impinge on the substrate very quickly, minimizing the potential for spray drying of the film (Qiu Y et al., 2009).

Fig.2. Process variables involved in Wurster-based coating process (\*Medium risk process variables, ¥ High risk process variable).



**Process variables involved in Wurster-based Coating Process**

The Wurster process have five sets of process variables affecting the quality of pellets - Equipment variables, solution preparation variables, preheating variables, spraying variables and drying variable (Fig.2) those are discussed in detail below.

**Air distribution plate (ADP)**

Suitable ADP has to be selected to get consistent fluidization at minimum attrition. The fluidization volume affects particle velocity; the smaller particle requires lesser air volume to attain certain height than the bigger particles. The air velocity and differential pressure at the air distribution plate must be almost same. Therefore, when deal with the smaller particle, use plate with lesser opening area to create the resistance at the ADP to have better distribution of the air (Shetty, 2010; Qiu Y et al., 2009). There are some recommendations for plate selection based on size of pellets or power (Table 1).

Table 1. Guideline for plate selection with respect to the final particle size

Equipment	Pellet size in micron	Plate combination
6" Wurster	< 500 Micron	A
	250 << 1200 Micron	B
	600 << 1800 Micron	C
	> 1200 Micron and Tablets	D
For commercial models	< 300 Micron	A – I
	150 << 800 Micron	B – I
	500 << 1200 Micron	B – H
	700 << 1400 Micron	C – H
	800 << 1800 Micron	C – G
	> 1500 Micron and Tablets	D - G

**Column height**

Appropriate adjustment of the partition gap ensures proper substrate circulation through the spray zone and up the partition column (Christensen and Bertelsen, 1997). The height of column changed based on the particle properties like size, shape, flow and bulk density. It was recognized as an important factor in determining the success of coating small substrates and was

found to affect the drug release profile of coated pellets (Porter and Ghebre-Sellassie, 1994). This was due to the pellets flow into the column and the exposure of pellets to the coating droplets in the spray zone (Fitzpatrick et al., 2003; Shelukar et al., 2000).

The slow and slugged form flow of particles through column leads to increased in agglomerates which column gap is too more and insufficient pressure differential created to draw particles in column. While, when gap is too small, less pellets draw in the column and coating material loss and chances of over wetting. Adjust the column height such a that maximum pellets comes in column. Frequently change in column height is not recommended. The recommended gap for 6" Wurster is 15-25 mm and for 18" Wurster is 40-50 mm.

**Nozzle tip diameter**

For the selection of nozzle, smaller the nozzle insert, more consistent will be spray. However smaller nozzle insert may cause nozzle choking. To avoid agglomeration in wurster coater the coating fluid is to be atomized more finely than in pan coater for tablets. It is necessary that the nozzle used in capable of atomizing the coating fluid even if the coating fluid delivery rate is increased. Large droplets of coating fluid generated by low performance nozzle does not distribute evenly over the material to be coated and do not dry quickly as smaller droplets. Very small droplets may dry quickly. Some droplets may contact tablets or beads surface but may dry before getting spread, it will result in to the irregular surface on core material. To maintain uniform atomization when spray rate exceeds the capacity of nozzle large droplets of coating fluid appears along with small droplets, large droplets results in to the formation of agglomerates. To avoid agglomeration multiple unit nozzles should be used (Harlan, 2004).

**Filter bags**

A filter bag is used to prevent loss of material and to allow air to pass through. If the porosity is higher than optimal, the loss of material will be high. If the porosity is lower than optimal, the filter will clog and processing will be interrupted which impact on the product yield.

A filter bag is selected based on particle size of material and previous experience. The porosity of

filter bag during coating can examine by monitoring differential pressure.

#### **Coating solution/suspension nature**

Coating solution/suspension should have enough solid content to easy spraying. If the viscosity of coating liquid is more it will affect on droplet size and change the pellets surface. The ideal coating liquid velocity should not be more than 250 mPa.s.

#### **Inlet and Product temperature**

The inlet drying air is usually heated before passing into the coating chamber to enhance the evaporation of coating material sprayed onto the cores. Control of the air temperature is important as it affects the quality of coats formed. Generally, excessively dry environment leads to spray drying effect and attrition while overwetting causes agglomeration (Maronga and Wnukowski, 1998). The optimal temperature allows the evaporation of solvent to take place at a rate that is sufficiently slow for adequate spreading of spray droplets and coalescence of polymer particles, and fast enough to avoid agglomeration and drug migration into the liquid layer (Yang and Ghebre-Sellassie, 1990). When the temperature of the air is too high, sprayed droplets dry quickly and do not coalesce when impinged on the core particles. This forms discontinuous coats which are rough and porous and will not impart the desired controlled release properties of a functional coat (Fukumori, 1994). The high temperatures may also cause spray drying of atomized droplets before they reach the cores, resulting in loss of coating material and thinner coats. Spray dried coating materials may also be embedded in the film coats, disrupting the continuity (Oliveira *et al.*, 1997; Ronsse *et al.*, 2007). On the other hand, when the temperature is too low, a longer time is required for coat drying and this allows soluble drug to migrate from the cores into the moistened coat layer. The dissolved drug reduces the surface tension of the liquid layer, lowering the capillary forces required for deformation and coalescence of spray droplets. Drug embedded in the resultant coat may dissolve on contact with dissolution media, resulting in a porous and more permeable coat. If the temperature is lower than the minimum film formation temperature, coalescing would not occur, resulting in discontinuous porous films (Oliveira *et al.*, 1997). In methacrylic acid based coating, at higher temperature spray gun choked frequently due to film formation of low glass

transition coating dispersion. So it recommended that run the methacrylic acid based coating below 30°C product temperature. While in aqueous ethylcellulose based coating required minimum 45°C product temperature due to high glass transition temperature of ethylcellulose polymer.

#### **Air volume**

Air volume is responsible for the circulation and drying of substrates during coating. Insufficient airflow may not provide sufficient drying air to circulate the substrates and remove the moisture from the deposited sprayed droplets during coating and consequently result in a high degree of agglomeration. However, excessively high airflow rates can increase attrition conditions causing erosion of friable cores or stress cracks in coats and may also augment the spray drying effect. For functional coats, this can result in loss of the desired release properties (Cole, 1995, Qiu Y *et al.*, 2009). The suitable airflow rate is unique for each coating equipment and also depends on product characteristics such as particle density, size, and shape (Christensen and Bertelsen, 1997). For non-aqueous coating a bubbling type of fluidization in down bed is suggested to minimize the generation of static charge and particle friction, whereas for aqueous coating more rigorous fluidization is needed to have more drying efficiency.

#### **Dew point**

In addition to the temperature, humidity of the inlet drying air also affects the drying of coated particles. The relationship between temperature and relative humidity or moisture content of air at different atmospheric pressures may be derived from psychometric charts (Shallcross, 1997). The humidity of air may vary from season to season or day to day. The changes in dew point of air changes the evaporating efficiency of that air. Lower humidity in the inlet air will enhance the drying capacity of air even at low temperature but it will cause excessive static charge in the product. To eliminate static charge and process variability, the required specific and absolute level must be set at the initial stage of development itself. Too high absolute humidity will result in a depression in air temperature below dew point, which will cause the condensation of water either on to machine or product substrate surface. It is not recommended to keep high moisture for a water soluble substrate at initial stage. The humidity can be increased after the initial coating

because the static charge develops only once the pellets are coated with polymers (McGinity, 2002). To maintain same environment in Wurster chamber during particle coating in lab scale or commercial batches, run the process at dew point mode. The dew point is scale independent factor.

### **Spray rate**

In Wurster binary nozzle are used. The droplet formation, spreading, coalescence and evaporation happen almost simultaneously during the process. The spray rate depends on the core particles as well as the solution properties. The evaporation occurs by atomization air used for the formation of spray mist which results in increase in the droplets viscosity. In case of solvent coating, sometime excessive atomization pressure leads to spray drying portion of spray. The spray rate has to be adjusted according to drying efficiency, tackiness of solution. To coat smaller particles we need to keep the droplet size small either by increasing the atomization pressure or by decreasing spray rate to avoid agglomeration. At the beginning of coating the spray rate must be kept low to avoid solubilizing the core, seepage of the drug or coating polymer in to other layer. Once the initial barrier formed, the spray rate can be increased up to the optimum level. It is known that as the particle becomes bigger it can take up more droplets without agglomerating. When the particle enlargement is too high we may require increasing the spray rate in a regular interval (Swarbrick and Boylan, 1992).

High spray rates increase the propensity for agglomeration and result in formation of less uniform coats, while low spray rates increase the coat uniformity (Singh et al., 1996). Low spray rates also enable smaller spray droplets to be formed which would reduce agglomeration, especially when coating smaller substrates (Jones and Percel, 1994). However, if the spray rate is too low, fast drying of the droplets could prevent coalescence of polymer particles, resulting in poorly formed coats (Heng et al., 1999).

### **Atomization air pressure**

Pneumatic nozzles are commonly used for spraying of coating materials in air suspension processes. These nozzles make use of air pressure to shear

the coating materials into atomized droplets. Higher atomizing air pressures result in smaller spray droplets (Wan et al., 1995) and are required to prevent agglomeration, especially when coating smaller substrates (Hemati et al., 2003). When the atomizing pressure is too high, the spray droplets can be propelled away too quickly and this does not promote droplet-core contact. High atomizing air pressure also increases the attrition of cores and can produce more fines. On the other hand, low atomizing pressure causes the formation of coarse spray droplets, which dry slowly and encourage the formation of liquid bridges between the cores, leading to increased agglomeration of the substrates being coated (Heng et al., 1999).

There is an important consideration in larger capacity equipment, where there may be significant drying capacity, and the rate limiting factor is the inability of the nozzle to atomize liquid (to a satisfactory droplet size) at the rate at which the process air may remove the resultant water vapor. The only possibility for taking advantage of the increased drying capacity is to enlarge the nozzle i.e. use more compressed air at the same pressure. A process that has excessive drying capacity, but is limited by droplet size, will result in unnecessarily hindered productivity. Upgrading to the HS nozzle, which uses substantially more compressed air at the same atomization air pressures (approximately three times the volume of the 940 series nozzle), will result in a dramatic improvement in drying capacity utilization.

### **Drying/curing time**

The polymers dissolved in organic solvent increased the solution viscosity. During film formation, gel like phase create during solvent evaporation and polymer film formed (Fig. 3a) (Muschert S, 2008). While in aqueous dispersions, film formation is more complicated (Fukumori, 1994). Surfactants, anti tacking agent and plasticizers are used aqueous dispersion to improve film nature and coating process. Plasticizers are used to reduce minimum film formation temperature (MFT) of polymers having high glass transition temperature (Tg) (Wheatley, 1997). In aqueous dispersions base coating, polymer particles come into contact with each other and form coalescence during drying (Paeratakul O, 1993).

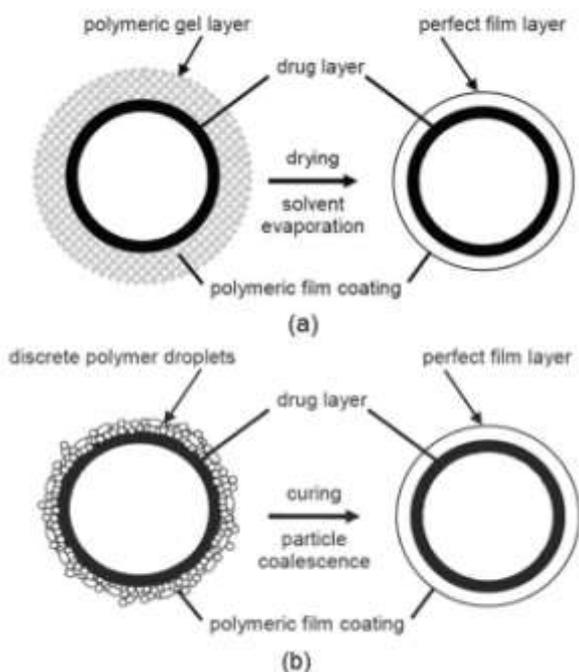


Fig. 3. a) Schematic presentation of the film forming mechanism from organic polymer solution b) Schematic presentation of the film forming mechanism from aqueous polymer dispersion

Usually the coating process is performed at sufficient high temperatures to guarantee softness of the discrete polymer particles. The softening is related to the glass transition temperature ( $T_g$ ) of the polymer (Augustine and York, 1988). A curing step (post coating thermal treatment) is carried out after coating process to assure complete film formation and avoid further gradual coalescence (Harris, 1997).

### Scale up process

The process parameters in the fluid beds are controllable precisely, which ensures easier optimization and reproducibility of the product quality. There are some wrong concepts related to Wurster based scale up process. There are number of articles available about Wurster processing, optimization and scale up. Mehta showed little correlation between load sizes; spray rate and process time, with total spraying time increasing at every scale over five different size chambers, both single and multiple nozzles (Mehta, 1988). Other published studies, which confirm reproducibility of coating applied also demonstrate a processing time increase of 5x and 3.1x for two different products scaled from small scale to manufacturing scale (3kg to 180kg).

Still question arises - "What would be the scaling up factor and consideration for reproducibility of the product quality in Wurster coating?". The

industry, which needs to scale up newly developed products from laboratory or research to manufacturing scale, must be aware of the proper designing for scaling up factor.

Currently FDA is focusing on the Quality by Design (QbD) concept where in one has to build the finished product quality attributes in the design itself. Nowadays USFDA also demanding for scientific approach for scale activity based on development batches. In one of the USFDA's guide to inspections report pre/post approval issues explained the expectations of regulatory authority on scale up activity said - it is important that the development and scale-up of the process be well documented so that a link between the bio/clinical batches and the commercial process can be established (USFDA, 1994).

Before attempt for successful scale up, key variables and their effect on the output should be identified during lab scale. If the scale up activity starts at the stage of development itself then it will be very easy to scale up and scale out the formulation. Wurster process has 'n' number of variables. Some of them are easy to establish e.g. batch size, spray liquid viscosity, concentration, spray assembly setting, base plate, column height and dew point etc. Perform some trials to fix some dependent variables like air volume, atomization air pressure, spray rate, product temperature etc. It is easy to understand the variables in small scale and it requires less time and cost. Finally apply design of experiments (DoE) to fix up most critical parameters as per regulatory requirement. To minimize the number of trials further one can use statistical software like Design-Expert software (Stat-Ease, Inc., Minneapolis, MN). From the output of the statistical analysis fix up the ranges for the parameter and validate the process to check the reproducibility and freeze the parameter. Once these variables are frozen, we are left with only one unknown factor - "mass effect" due to increase in the batch weight from lab scale to commercial scale. Once the parameters are studied then it will be easier to compensate the mass effect by doing minor changes in the predicted parameter in pilot and commercial level. After freezing the parameters at lab model next step is predicting the parameter for scale up.

Since, at least 3 successful reproducible development batches done then next step is to set

up parameters for pilot batch also have single Wurster. The development of the product is normally done 6" wurster with the batch size 0.5 to 2 kg. The wurster column and spray nozzle is small. Overall coating zone is small. The recommended pilot model is 18" wurster where the wurster column and base plate are much larger. From the lab to pilot although there is single spray nozzle but the nozzle is much bigger and can permit higher spray rate. The batch depth and mass flow density increases. Overall, the coating zone increases from lab to pilot scale. The overall coating zone will remain same in pilot and commercial scale except the height of the wurster column. Therefore, base area of wurster column plays important role in efficient coating. All process parameters should be proportional to the base area of wurster column compared with lab model column.

All the process variables again show their significance in scale up model also. Nevertheless, once the effect of variables are studied and understood in lab model it will make the analysis much easier. Just like the variables remaining same in pilot scale also, the same process control will apply. Only the unknown factor will be the mass effect. As in the lab scale, one has to follow sequential approach to set the parameter for the scale up.

Linear scale up from lab scale to pilot scale assumed that the occupancy are the same and the distribution plate in each piece of equipment is geometrically similar. Additionally, ratios of air volume to plate area and spray rate to air volume maintained. The scale up factor from Pam GPCG 1.1 to Pam FBE 125C is approximately 9-fold based on vendor recommendation. This scale up factor is applicable for air volume, spray rate and atomization air pressure.

The variables considered during successful scale up batch in Wurster are discussed below.

#### **Batch size**

First step to design pilot scale up after deciding equipment is defining the batch size. The process parameter may change slightly depending on the batch size due to mass effect. Set and validate the process for any change in the batch size. Keep the batch size within the recommended occupancy. e.g. For Pam GPCG 1.1, the working volume is 2.4 liter, where as Pam FBE 125 it is 84 liter, i.e. 35

times. If pilot scale up planned in FBE 125C then batch size should be 35 times of batch size taken in GPCG 1.1 (Table 2). Working volume of batch at initial and final stage should be in 20 to 100% for non functional coating and 20 to 80% for functional coating limit.

#### **Air volume**

Fluidization pattern during processing is depending on air volume. The air volume of scale up batch decided based on optimized lab scale batch. From lab to pilot scale the face velocity must be kept same. To maintain the same velocity one must know the base plate area under column of lab and pilot equipment. It is expressed in the term of fluidization air volume. Following equation can be used to calculate the Airflow.

$$V_2 = V_1 \times A_2 / A_1$$

Where,  $V_1$  =Air flow at Lab model,  $V_2$  =Air flow for scale up model,  $A_1$  = Base area of wurster column for lab model,  $A_2$  = Base area of wurster column for pilot model.

#### **Spray rate and atomization air pressure**

The increase in the spray rate shall be always in the line of increase in the drying capacity rather than the batch size. The spray rate for a product is typically a key variable, from several perspectives. The first is economic-long processes result in high manufacturing costs. Lengthy processes also increase the likelihood of problems during the process, particularly nozzle port clogging. The spray rate is increased in related to increase in inlet air volume. Drying capacity is critical component consider in scale up activity. The drying capacity, batch size, core material and droplet size of coating liquid in coating zone are the rate limiting factors. Being said the inlet air humidity and temperature will remain same for the scale up model, the drying efficiency is increased only it terms of air volume. The spray rate can be increased in the same fold increase in the inlet air volume. spray nozzle with HS Wurster has benefits over conventional coating gun. The droplet size is large near the tip of spray gun which formed agglomerated while by accommodating HS Wurster, material not comes in contact with coating gun and spray rate can increased more. Following equation used to calculate to predict the spray rate in pilot model.

$$S_2 = S_1 \times V_2 / V_1$$

We can also say that  $S_2 = S_1 \times A_2/A_1$   
 Where,  $V_1$  =Air flow at lab model  $V_2$  =Air flow for scale up model,  $S_1$  =Spray rate in Lab model,  $S_2$  =Spray rate in pilot model  
 The increase in the spray rate must be compensated with the increase in the atomization air pressure to maintain the droplet size of the spray mist. To keep the droplet size same both in

18" to 32" or more capacity Wurster is simpler due to bed height is almost same.

**Theoretical parameters**

Since product temperature and dew point are most critical factors that have an impact on the product movement as well as release profile, during scaling up these parameters should be kept

Table 2. Comparative pellets coating process parameters of Pam GPCG 1.1 and Pam FBE based on scale up factor

Parameters	Units	Pam GPCG 1.1	Scale up factor	Pam FBE 125 C
<b>Equipment Parameters</b>				
Wurster column diameter	m	0.072	-	0.219
Wurster column height	m	0.20	-	0.36
Base plate area	m <sup>2</sup>	0.0145	-	0.1918
Suitable air distribution plate	-	B	-	B-I
Working volume	Litre	2.4	35	84
Batch size (preferred)	Kg	0.6	35	21.0
Wurster column base area	m <sup>2</sup>	0.0041	9	0.0377
<b>Process Parameters</b>				
Inlet air temperature	°C	26-35	-	26-35
Product temperature	°C	26-28	-	26-28
Wurster column height from base plate	mm	15-20	-	40-45
Inlet air volume	CFM	9	9	81
Spray rate	gm/min	10-20	9	90-180
Spray gun model	-	970/0		940-943/7-1 S91
Atomization air pressure	bar (CFM)*	1.0 (1.2)	9	2.5 (10.8)
		1.5 (1.4)	9	3.0 (12.6)
		2.0 (1.7)	9	4.0 (15.3)

\*bar to CFM calculation performed based on type of spray gun. CFM value was scale up

lab as well as pilot model one has to keep the spray rate to atomization air volume same. Normally atomization air volume should restrict them maximum pressure up to 4 to 5 bar. Higher the atomization air pressure the mechanical stress on the core will be high due to higher velocity. If someone uses higher air pressure in lab model then during the scale up either the spray rate needs to be reduced or the spray gun with higher capacity like HS gun can be used. Any deviation in the spray rate from the scale up factor of airflow shall be compensated by either increasing or reducing the inlet air temperature.

**Mass effects**

Mass effect can't predict based on batch performance in small scale equipment. The best scale up of Wurster process is from 6" lab model to 18" industrial scale model. In 6" Wurster, bed height not more than 200 mm and material fluidized up to 125 cm or less height. In the 18" Wurster, bed height is up to 600 mm, and fluidization height up to 2 meters. Scale up from

constant. There may be some deviation in the results from lab scale even after maintaining the parameters as per the scale up calculations due to mass effect. One or the other parameter may have to be changed marginally to achieve desired release profile. The scale up activity starts with preliminary trials with predicted parameter, analyze the results, and take action if required to match the profile. If all the parameter and their effect on the release were understood in the lab scale, it will be easier to analyze the analytical results and vary the parameters to get desired profile. Process validation is recommended to check the robustness of the process before filing the parameters or planning the scale out activity.

**Case study**

Successful lab scale batch was taken in Pam GPCG 1.1 (6" Wurster) of pellet core of 200-300 micron which increased up to 500 micron after functional coating. If scale up planned in Pam FBE 125 which has single partition column, then 9 will be the scale

up factor based on Wurster column base area comparison. Following are the values of process parameters obtained for FBE 125 C based on scale up factor to get reproducible results.

### Conclusion

Wurster based coating process involved air volume, product temperature, spray rate and atomization air pressure are the high risk process variables which can mitigate by systematic optimization study while column height, filter bag type, dew point and drying time are medium risk process variables which can fix during lab scale batches. Many reported difficulties in scaling up a process can be traced to improper correlation of these factors and/or to poor equipment design. The best approach to start the scaling up activity is to collect complete information about the equipment from the manufacturer in the beginning itself.

### References

- [1] Bhad, M. E., Shajan, A., Jaiswal, S. B., Chandewar, A. V., Jain, J. M., & Sakarkar, D. M. (2010). MUPS Tablets – A Brief Review. *International Journal of PharmTech Research*, 2 (1), 847-855.
- [2] Christensen, F. N., & Bertelson, P. (1997). Qualitative description of the Wurster-based fluid-bed coating process. *Drug Development and Industrial Pharmacy*, 23(5), 451-463.
- [3] Cole, G. C. (1995). Coating pans and coating columns. In: Cole, G. C. (Ed.), *Pharmaceutical Coating Technology*. London: Taylor and Francis. p. 205-239.
- [4] Deb, R., & Ahmed, A. B. (2013) Pellets and Pelletization techniques : A critical review. *International Research Journal of Pharmacy*, 4(4), 90-95.
- [5] Dey, N. S., Majumdar, S., & Rao, M. E. B. (2008) Multiparticulate drug delivery system for controlled release. *Tropical Journal of Pharmaceutical Research*, 7(3), 1067-1075.
- [6] Fitzpatrick, S., Ding, Y., Seiler, C., Lovegrove, C., Booth, S., Forster, R., Parker, D., & Seville, J.(2003). Positron emission particle tracking studies of a Wurster process for coating applications. *Pharmaceutical Technology*, 27(9), 70-78.
- [7] Fukumori, Y. (1994). Coating of multiparticulates using polymeric dispersions. In: Ghebre-Sellassie, I. (Ed.), *Multiparticulate Oral Drug Delivery*. New York: Marcel Dekker. p. 79-112.
- [8] Harlan, S.H. (2004). Scaling of fluid bed coating. *Pharmaceutical Technology*, 96-102.
- [9] Harris, M. R. (1997). Aqueous polymeric coating for modified release oral dosage forms. In: McGinity, J.W. (Ed.), *Aqueous polymeric film coatings for pharmaceutical dosage forms*. Marcel Dekker, New York, p. 81-100.
- [10] Hemati, M., Cherif, R., Saleh, K., & Pont, V. (2003). Fluidized bed coating and granulation: influence of process-related variables and physicochemical properties on the growth kinetics. *Powder Technology*, 130, 18– 34.
- [11] Heng, P.W.S., Chan, L.W., & Chan, W.Y. (1999). Application of spot colour measurement for the optimization of colour coating. *STP Pharma Science*, 9, 539-544.
- [12] <http://www.fda.gov/ICECI/Inspections/InspectionGuides/ucm074928.htm> Accessed 18 Sept 2014.
- [13] Jones, D. M., & Percel, P.J.(1994). Coating of multiparticulates using molten materials: Formulation and process considerations. In: Ghebre-Sellassie, I. (Ed.), *Multiparticulate Oral Drug Delivery*. New York: Marcel Dekker. p.113-142.
- [14] Maronga, S. J., & Wnukowski, P. (1998). The use of humidity and temperature profiles in optimizing the size of fluidized bed in a coating process. *Chemical Engineering and Processing: Process Intensification*, 37(5), 423–432.
- [15] McGinity, J. W., Mehta, K. A., & Frisbee, S. E. (2002). Processing factors that influence the in vitro in vivo performance of film coated drug delivery system. *Drug Delivery*, 2002, 2, 72-76.
- [16] Mehta, A. M. (1988). Scale-up Considerations in the fluid-bed Process for Controlled Release Product. *Pharmaceutical Technology*, 12, 46-52.
- [17] Mohamad, A., Dashevsky, A. (2006). Development of pulsatile multiparticulate drug delivery system coated with aqueous dispersion Aquacoat ECD. *International Journal of Pharmaceutics*, 318(1-2), 124–131.
- [18] Muschert, S. (2008). Polymeric coatings for solid dosage forms: characterization and optimization. Thesis. Universite de Lille II, Lille.
- [19] Okhamafe, A. O., & York, P.(1988). Studies of interaction phenomena in aqueous-based film coatings containing soluble additives using thermal analysis techniques. *Journal of Pharmaceutical Science*, 77(5), 438-443.
- [20] Oliveira, W.P., Freire, J.T., & Coury, J.R. (1997). Analysis of particle coating by spouted bed process. *International Journal of Pharmaceutics*, 158(1), 1-9.
- [21] Pan, X., Chen, M., Han, K., Peng, X., Wen, X., Chen, B., Wang, J., Li, G., & Wu, C. (2010). Novel compaction techniques with pellet-containing granules. *European Journal of Pharmaceutics and Biopharmaceutics*, 75(3), 436–442.
- [22] Paeratakul, O. (1993). Pharmaceutical applications of aqueous colloidal polymer dispersions. Thesis. University of Texas: Austin.
- [23] Porter, S.C., Ghebre-Sellassie, I. (1994). Key factors in the development of modified release pellets. In: I. Ghebre-Sellassie (Ed.), *Multiparticulate Oral*

- [24] Drug Delivery. New York: Marcel Dekker. p. 159-180.
- [25] Qiu, Y., Chen, Y., Zhang, G. G. Z., Liu, L. & Porter W. R. (2009). Developing Solid Oral Dosage Forms : Pharmaceutical Theory And Practice. In: Jones, D, Development, Optimization, and Scale-up of Process Parameters Wurster Coating. Academic press. p. 807-825.
- [26] Ronsse, F., Pieters, J. G., & Dewettinck, K. (2007). Combined population balance and thermodynamic modeling of the batch top-spray fluidised bed coating process. Part I Model development and validation. *Journal of Food and Engineering*, 78, 296-307.
- [27] Singh, S. K., Reddy, I. K., & Khan, M. A. (1996). Optimization and characterization of controlled release pellets coated with an experimental latex: II. Cationic drug. *International Journal of Pharmaceutics*, 141(1-2), 179-95.
- [28] Shajahan, A., Chandewar, A. V., & Jaiswal, S. B. (2010). A flexible technology for modified-release drugs: multiple-unit pellet system (MUPS). *Journal of Controlled Release*, 147, 2–16.
- [29] Shallcross, D. C. (1997). Psychrometric charts. In: Shallcross, D. C. (Ed.), *Handbook of psychrometric charts: humidity diagrams for engineers*. London: Blackie Academic and Professional. p. 44-45.
- [30] Shelukar, S., Ho, J., Zega, J., Roland, E., Yeh, N., Quiram, D., Nole, A., Katdare, A., & Reynolds, S. (2000). Identification and characterization of factors controlling tablet coating uniformity in a Wurster coating process. *Powder Technology*, 110 (1-2), 29-36.
- [31] Shetty, V. (2010). Wurster Coating - Scale up and Scale out. *Pharma Times*, 42, 33-37.
- [32] Swarbrick, J., Boylan, J. C. (1992). *Encyclopaedia of Pharmaceutical Technology*. Vol 6. New York: Marcel Dekker Inc. p.171-176.
- [33] Tuleu, C., Andrieux, C., Boy, P., & Chaumeil, J. C. (1999). Gastrointestinal transit of pellets in rats: effect of size and density. *International Journal of Pharmaceutics*, 180(1), 123–131.
- [34] Varum, F. J., Merchant, H. A., & Basit, A. W. (2010). Oral modified-release formulations in motion: the relationship between gastrointestinal transit and drug absorption. *International Journal of Pharmaceutics*, 395(1-2), 26–36.
- [35] Wan, L. S. C., Heng, P. W. S., & Liew, C. V. (1995). The influence of liquid spray rate and atomizing pressure on the size of spray droplets and spheroids. *International Journal of Pharmaceutics*, 118 (2), 213-219.
- [36] Wheatley, T. A. (1997). Latex emulsion for controlled drug delivery. In: McGinity, J.W. (Ed.), *Aqueous Polymeric Coatings for Pharmaceutical Dosage Forms*. Marcel Dekker, New York, 1997, p.1-54.
- [37] Yang, S.T., & Ghebre-Sellassie, I. (1990). The effect of product bed temperature on the microstructure of Aquacoat-based controlled-release coatings. *International Journal of Pharmaceutics*, 60(2), 109-124.